

Modelling Drifts in Receiver Calibrations for Global 21-cm Cosmology Experiments

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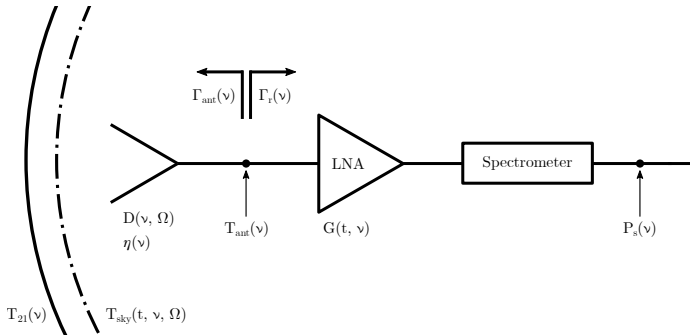


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Global Experiment Receiver System



- Low Noise Amplifier (LNA) with gain G outputs amplified power

What Is Calibration?

- Calibration relates output power spectral density (PSD) to temperature
- In general this relation can be written as

$$P_{\text{source}} = kBgM(T_{\text{source}} + T_{\text{rec}}) \quad (1)$$

- g is the source independent gain of the low noise amplifier (LNA) and M is the impedance mismatch factor
- T_{rec} is added noise temperature from LNA



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Characterising the LNA with Noise Waves

- When the sources are not impedance matched M and T_{rec} are *source dependent* – simple Dicke switching cannot be used
- One way to characterise the LNA is using ‘noise waves’ (Meys, 1978; Monsalve et al., 2017)

$$T'_{\text{NS}} \left(\frac{P_s - P_L}{P_{\text{NS}} - P_L} \right) + T'_L = T_s \left[\frac{1 - |\Gamma_s|^2}{|1 - \Gamma_s \Gamma_r|^2} \right] + T_{\text{unc}} \left[\frac{|\Gamma_s|^2}{|1 - \Gamma_s \Gamma_r|^2} \right] \\ + T_{\text{cos}} \left[\frac{\text{Re} \left(\frac{\Gamma_s}{1 - \Gamma_s \Gamma_r} \right)}{\sqrt{1 - |\Gamma_r|^2}} \right] + T_{\text{sin}} \left[\frac{\text{Im} \left(\frac{\Gamma_s}{1 - \Gamma_s \Gamma_r} \right)}{\sqrt{1 - |\Gamma_r|^2}} \right] \quad (2)$$

- “Calibration equation” - three noise wave parameters: T_{unc} , T_{cos} , T_{sin}
- We also fit for T'_{NS} , T'_L (Roque et al., 2021)



Degeneracies in the Noise Wave Parameters

- Fitting for T'_{NS} and T'_L fits for the mismatch in reflection coefficients, however introduces degeneracies

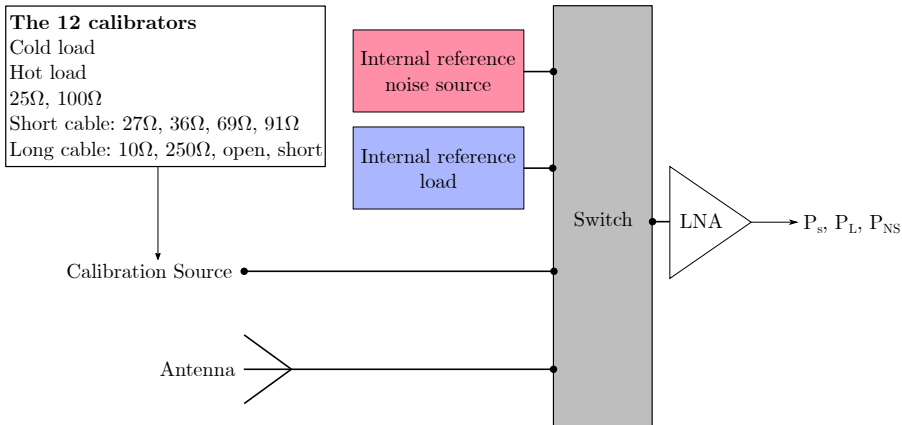
$$\begin{aligned}
 T'_{\text{NS}} = \frac{1}{1 - |\Gamma_{\text{rec}}|^2} & \left[T_{\text{NS}} (1 - |\Gamma_{\text{NS}}|^2) |F_{\text{NS}}|^2 - T_L (1 - |\Gamma_L|^2) |F_L|^2 \right. \\
 & + T_{\text{unc}} \left(|\Gamma_{\text{NS}}|^2 |F_{\text{NS}}|^2 - |\Gamma_L|^2 |F_L|^2 \right) \\
 & + T_{\text{cos}} \left(|\Gamma_{\text{NS}}| |F_{\text{NS}}| \cos \alpha_{\text{NS}} - |\Gamma_L| |F_L| \cos \alpha_L \right) \\
 & \left. + T_{\text{sin}} \left(|\Gamma_{\text{NS}}| |F_{\text{NS}}| \sin \alpha_{\text{NS}} - |\Gamma_L| |F_L| \sin \alpha_L \right) \right]
 \end{aligned} \tag{3}$$

and

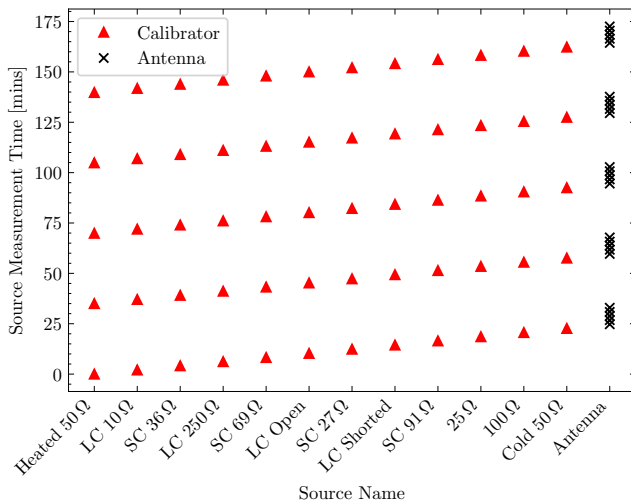
$$\begin{aligned}
 T'_L = \frac{1}{1 - |\Gamma_{\text{rec}}|^2} & \left[T_L (1 - |\Gamma_L|^2) |F_L|^2 + T_{\text{unc}} |\Gamma_L|^2 |F_L|^2 \right. \\
 & \left. + T_{\text{cos}} |\Gamma_L| |F_L| \cos \alpha_L + T_{\text{sin}} |\Gamma_L| |F_L| \sin \alpha_L \right]
 \end{aligned} \tag{4}$$



REACH Receiver



REACH Observations



Exploiting the Linearity

- All measured quantities – PSDs, reflection coefficients – absorbed into X terms to give

$$T_s(\nu) = X_{\text{unc}} T_{\text{unc}} + X_{\text{cos}} T_{\text{cos}} + X_{\text{sin}} T_{\text{sin}} + X_{\text{NS}} T_{\text{NS}} + X_{\text{L}} T_{\text{L}} \quad (5)$$

- Can write this as a linear equation

$$\mathbf{T}_s = \mathbf{X}\mathbf{\Theta} + \sigma \quad (6)$$

- *measured* – $\mathbf{X} = \begin{pmatrix} X_{\text{unc}} & X_{\text{cos}} & X_{\text{sin}} & X_{\text{NS}} & X_{\text{L}} \end{pmatrix}$
fitted for – $\mathbf{\Theta} = \begin{pmatrix} T_{\text{unc}} & T_{\text{cos}} & T_{\text{sin}} & T_{\text{NS}} & T_{\text{L}} \end{pmatrix}^T$



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Calibration Likelihood

- For this talk we will use a Gaussian Likelihood

$$\mathcal{L} = \frac{1}{\sqrt{|2\pi\mathbf{C}|}} \exp \left\{ -\frac{1}{2}(\mathbf{T} - \mathbf{X}\Theta)^T \mathbf{C}^{-1}(\mathbf{T} - \mathbf{X}\Theta) \right\} \quad (7)$$

- Where Θ are the model coefficients
- Sample the posterior distribution analytically using the conjugate priors method (Roque et al., [2021](#))
- Calibration solution is the weighted mean of posterior



Surface Fitting

- We fit a polynomial frequency-time surface

$$T_{\text{NWP}}(\nu, t) = \sum_i \sum_j A_{ij} \cdot \nu^i t^j \quad (8)$$

- Which can be written linearly as

$$\mathbf{T}_i = \mathbf{X}_i \mathbf{B}_i \Theta \quad (9)$$

where

$$\Theta = \begin{pmatrix} A_{00} \\ A_{01} \\ A_{10} \\ A_{11} \\ A_{02} \\ \vdots \end{pmatrix}, \mathbf{B}_i = \begin{pmatrix} 1 & t_i & \nu_0 & \nu_0 t_i & t_i^2 & \dots \\ 1 & t_i & \nu_1 & \nu_1 t_i & t_i^2 & \dots \\ 1 & t_i & \nu_2 & \nu_2 t_i & t_i^2 & \dots \\ \vdots & \vdots & \vdots & \vdots & \vdots & \ddots \end{pmatrix} \quad (10)$$

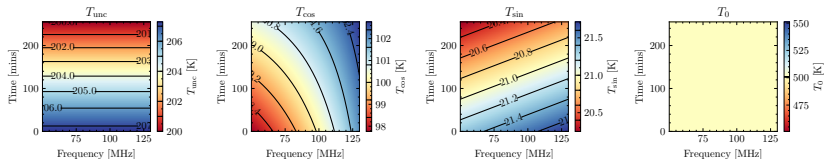


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Data Simulation



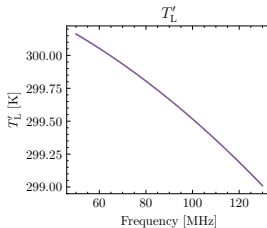
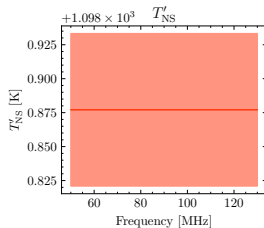
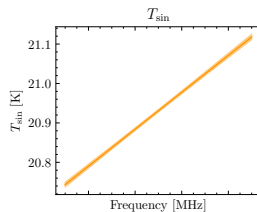
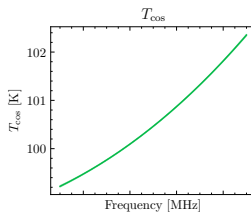
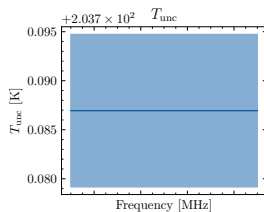
$$\begin{aligned}
 P_s = & kBg(T_s(1 - |\Gamma_s|^2)|F_s|^2 + T_{\text{unc}}|\Gamma_s|^2|F_s|^2 \\
 & + T_{\text{cos}}\text{Re}(\Gamma_s F_s) + T_{\text{sin}}\text{Im}(\Gamma_s F_s) + T_0)
 \end{aligned} \tag{11}$$

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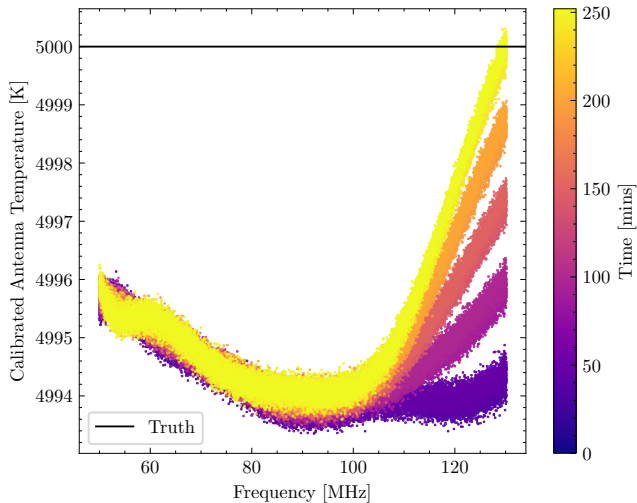
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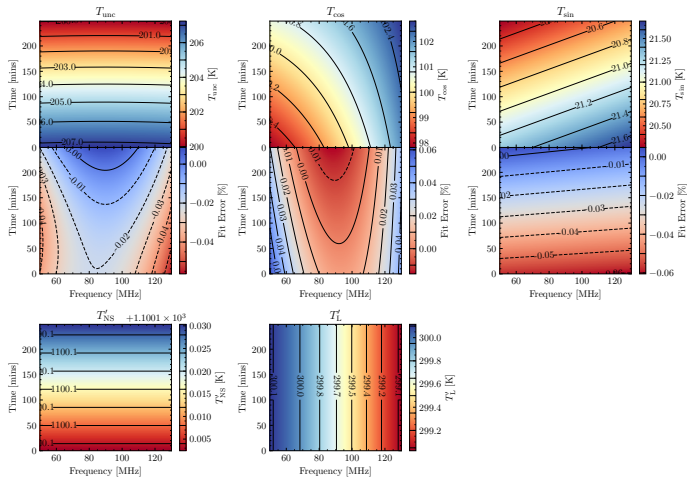
1-D Conjugate Priors



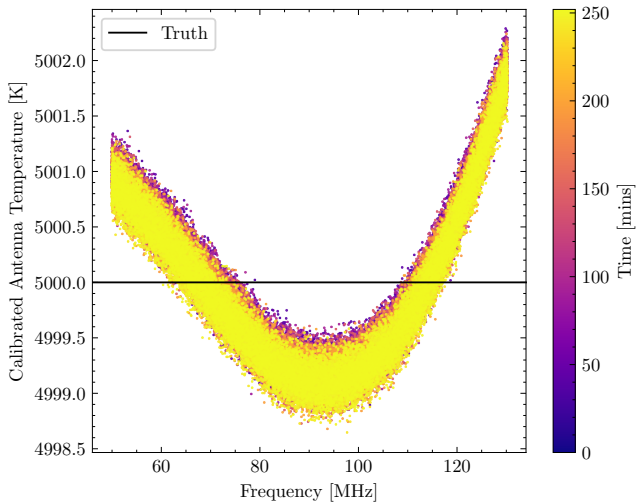
1-D Conjugate Priors



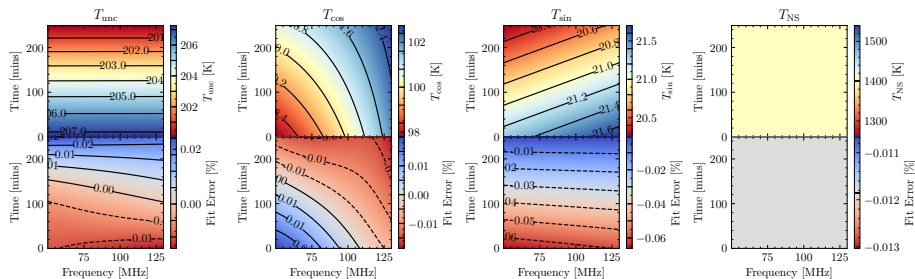
Surface Fitting



Surface Fitting



Surface Fitting Including Γ_L and Γ_{NS} Terms



Surface Fitting Including Γ_L and Γ_{NS} Terms

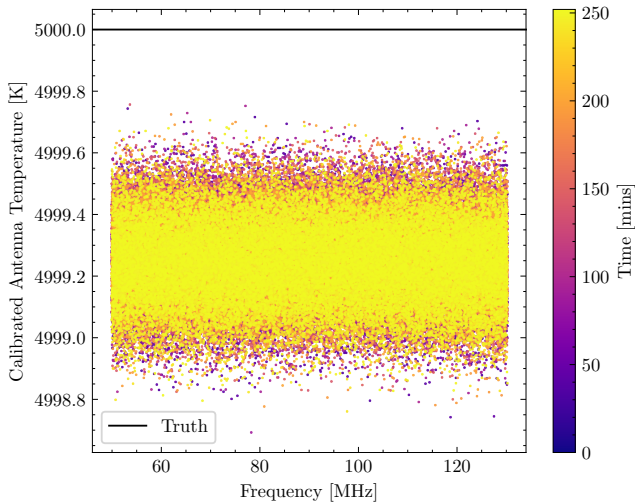
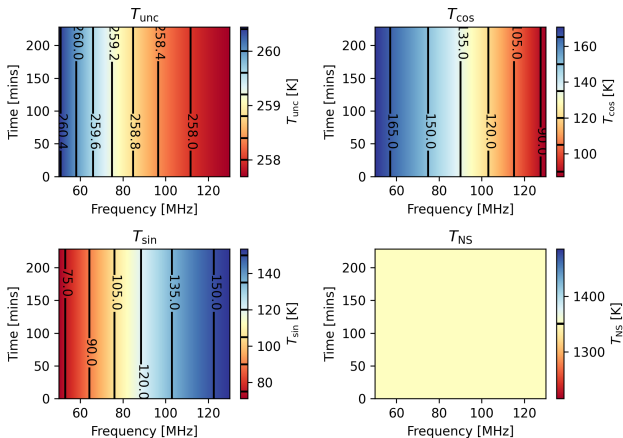


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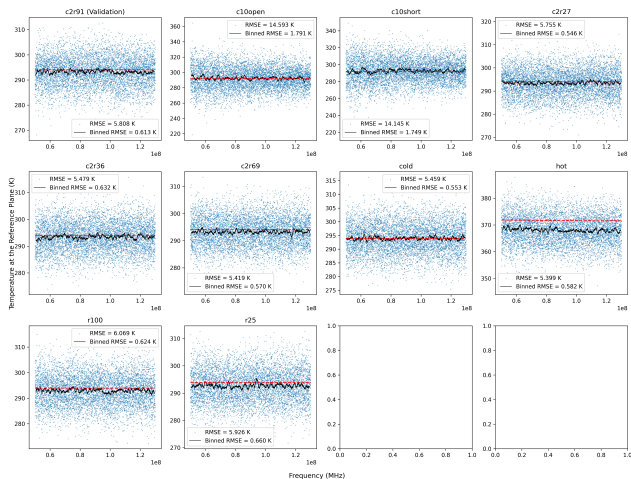
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Fitting REACH Data



Fitting REACH Data



Summary

- If the state of the receiver is drifting over the course of an observation it is necessary to consider this time change
- Fitting a frequency-time polynomial surface to simulated data removes drifts in the calibrated antenna solution but a leaves a significant chromatic residual
- Mitigating degeneracies by explicitly including Γ_L and Γ_{NS} terms removes this chromatic residual
- Tests on data from the REACH instrument show that the REACH receiver is not drifting over an observation



Extra: Calibration Equation with Γ_{NS} and Γ_L Terms

$$T_S(\nu) = \bar{X}_{unc} T_{unc} + \bar{X}_{cos} T_{cos} + \bar{X}_{sin} T_{sin} + \bar{X}_{NS} T_{NS} + \bar{X}_L T_L, \quad (12)$$

where

$$\bar{X}_{NS} = \frac{P_S - P_L}{P_{NS} - P_L} \frac{(1 - |\Gamma_{NS}|^2)|1 - \Gamma_S \Gamma_{rec}|^2}{(1 - |\Gamma_S|^2)|1 - \Gamma_{NS} \Gamma_{rec}|^2}, \quad (13)$$

$$\bar{X}_L = \left[1 - \frac{P_S - P_L}{P_{NS} - P_L} \right] \frac{(1 - |\Gamma_L|^2)|1 - \Gamma_S \Gamma_{rec}|^2}{(1 - |\Gamma_S|^2)|1 - \Gamma_L \Gamma_{rec}|^2}, \quad (14)$$

$$\bar{X}_{unc} = \bar{X}_{NS} \frac{|\Gamma_{NS}|^2}{1 - |\Gamma_{NS}|^2} + \bar{X}_L \frac{|\Gamma_L|^2}{1 - |\Gamma_L|^2} - \frac{|\Gamma_S|^2}{1 - |\Gamma_S|^2}, \quad (15)$$

$$\begin{aligned} \bar{X}_{cos} = & \bar{X}_{NS} \cdot \operatorname{Re} \left(\frac{\Gamma_{NS}}{1 - \Gamma_{NS} \Gamma_{rec}} \cdot \frac{|1 - \Gamma_{NS} \Gamma_{rec}|^2}{\sqrt{1 - |\Gamma_{rec}|^2}(1 - |\Gamma_{NS}|^2)} \right) + \bar{X}_L \cdot \operatorname{Re} \left(\frac{\Gamma_L}{1 - \Gamma_L \Gamma_{rec}} \cdot \frac{|1 - \Gamma_L \Gamma_{rec}|^2}{\sqrt{1 - |\Gamma_{rec}|^2}(1 - |\Gamma_L|^2)} \right) \\ & - \operatorname{Re} \left(\frac{\Gamma_S}{1 - \Gamma_S \Gamma_{rec}} \cdot \frac{|1 - \Gamma_S \Gamma_{rec}|^2}{\sqrt{1 - |\Gamma_{rec}|^2}(1 - |\Gamma_S|^2)} \right), \end{aligned} \quad (16)$$

$$\begin{aligned} \bar{X}_{sin} = & \bar{X}_{NS} \cdot \operatorname{Im} \left(\frac{\Gamma_{NS}}{1 - \Gamma_{NS} \Gamma_{rec}} \cdot \frac{|1 - \Gamma_{NS} \Gamma_{rec}|^2}{\sqrt{1 - |\Gamma_{rec}|^2}(1 - |\Gamma_{NS}|^2)} \right) + \bar{X}_L \cdot \operatorname{Im} \left(\frac{\Gamma_L}{1 - \Gamma_L \Gamma_{rec}} \cdot \frac{|1 - \Gamma_L \Gamma_{rec}|^2}{\sqrt{1 - |\Gamma_{rec}|^2}(1 - |\Gamma_L|^2)} \right) \\ & - \operatorname{Im} \left(\frac{\Gamma_S}{1 - \Gamma_S \Gamma_{rec}} \cdot \frac{|1 - \Gamma_S \Gamma_{rec}|^2}{\sqrt{1 - |\Gamma_{rec}|^2}(1 - |\Gamma_S|^2)} \right). \end{aligned} \quad (17)$$



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